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1	A four-experiment examination of ankle kinetics, kinematics and lateral ligament
2	strains during different conditions; an examination using musculoskeletal simulation.
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16	Keywords: Ankle ligament; kinematics; musculoskeletal stimulation; footwear; ankle braces.
17	Abstract
18	PURPOSE: Firstly, to provide insight into the differences in ankle kinetics, kinematics and
19	lateral ligament strain between males and females during functional sports movements. In
20	addition, this study explores the prophylactic efficacy of different footwear and bracing
21	modalities.
22	METHODS: Experiment 1 examined male and female athletes performing run, 45° cut and
23	one-legged hop movements, experiment 2 observed court, energy return and trainer footwear
24	conditions during a change of direction task, experiment 3 examined high-cut, low-cut and
25	trainer footwear conditions in change of direction, run, 45° cut and vertical jump movements

and experiment 4 explored an ankle sleeve and an ankle brace during a change of direction
movement. In each experiment ankle kinetics and ligament strain were measured using a
musculoskeletal simulation approach.

RESULTS: Experiment 1 indicates that males exhibited increased inversion velocity 29 (male=260.39 & female=219.18°/s) in the cut movement as well as enhanced peak posterior 30 force (male=2.24 & female=1.35BW), anterior talofibular ligament (ATFL) strain rate 31 32 (male=266.77 & female=133.16%/s). Experiment 2 showed that both calcaneofibular ligament (CFL) and posterior talofibular ligament (PTFL) strain velocities were greater in the court 33 footwear (CFL=90.86 & PTFL=151.45%/s) compared to the trainer (CFL=69.07 & 34 PTFL=119.57%/s). Experiment 3 showed in the run movement anterior talofibular ligament 35 (ATFL) strain was enhanced in the trainer (7.86%) compared to the high (3.61%) and low 36 37 (5.87%) conditions and the trainer (8.14%) compared to the low footwear (5.39%) for the cut movement. PTFL strain velocity was greater in the high footwear (188.01%/s) compared to the 38 trainer (175.60%/s) during the run movement and in both high (221.55%/s) and low 39 (220.29%/s) footwear compared to the trainer (202.05%/s) during the cut. Experiment 4 40 revealed that PTFL strain was greater in the sleeve condition (17.05%) compared to the ankle 41 brace (15.42%). 42

43 CONCLUSION: This study provides insight into the potentially increased incidence of lateral
44 ankle ligament sprain injuries in males, whilst also highlighting the prophylactic efficacy of
45 ankle braces in attenuating the ankle strain mechanisms linked to the aetiology of lateral ankle
46 ligament injuries.

47 Introduction

The benefits of physical activity/ sport are universally recognized; however, sports/ physical activity is associated with a high incidence of injuries (1). Ankle sprains are an extremely common complaint among physically active individuals, particularly in court based athletic disciplines (2-3). Lateral ankle sprains have been shown to account for 14% of all orthopedic
emergency cases (4), with an estimated 2.15 ankle sprains occurring per 1000-person years (5).
The most frequently injured lateral ankle ligaments are the anterior talofibular ligament
(ATFL), calcaneofibular ligament (CFL) and posterior talofibular ligament (PTFL) (6).
Importantly, many patients develop long lasting problems after experiencing an ankle sprain;
a condition broadly termed as chronic ankle instability (CAI) (7), and concerningly, 13% of
individuals with a history of CAI go on to experience post-traumatic ankle osteoarthritis (8).

The main function of skeletal ligaments is to maintain passive joint congruency (9), 58 59 however ligaments are also able respond to mechanical stimuli and provide proprioception and kinesthesia (10). Ligaments themselves are composed primarily of collagen fibers that 60 encompass approximately 75% of the dry ligamentous mass with proteoglycans, elastin, 61 62 glycoproteins and other proteins making up the remaining 25% (11). Sprain injuries experienced by the lateral ankle ligaments are mediated when excessive tension is applied to 63 the ligaments during athletic movements, this causes the ligaments collagen fibers to elongate 64 i.e. experience strain (9). Ligament injury can happen with a single acute episode which 65 exceeds the ligaments maximum strain capacity resulting in a ligament rupture, or from 66 cumulative overload with insufficient recovery time so that these chronic insults render the 67 ligaments unable to properly support the joint, leading to instability and pain (12). 68

Because of the high incidence of lateral ankle sprain injuries (4) and the poor-long term prognosis following injury (7), prophylactic/ preventative strategies are a key priority for clinical sports research (13). The ankle joint can theoretically be supported by external equipment (14), therefore devices such as ankle braces and sleeves as well as athletic footwear with different collar heights and traction characteristics have received considerable attention. To this end court-based footwear are designed with high-cut ankle supports designed primarily to limit excessive ankle movement (15). The biomechanical analyses examining the effects of

high cut footwear have provided contradictory results. In 45° cutting movements Commons & 76 Low (16) showed that high-cut footwear increased the peak ankle inversion angle whereas Lam 77 et al., (15) and Liu et al., (17) found that the ankle inversion angle and peak inversion velocity 78 were reduced in high-cut footwear. In addition, Klem et al., (18) showed during a 45° cutting 79 movement that a hinged ankle brace reduced peak inversion, dorsiflexion and compressive 80 loading compared to no-brace. Similarly, Graydon et al., (14) found that ankle braces 81 82 significantly reduced both sagittal and coronal plane movement of the ankle during running and Ubell et al., (19) revealed that ankle braces significantly enhanced participants ability 83 restrict inversion below a threshold of 24° during a one-legged jump task. Similarly, high 84 friction at the shoe-surface interface is a well-acknowledged risk factor for lateral ankle sprain 85 injuries (20), although to our knowledge there has yet to be any investigation which has 86 87 examined the effects of footwear with different frictional characteristics on the factors linked to the aetiology of lateral ankle strains. However, despite the wealth of biomechanical analyses 88 investigating effects of external prophylactic devices on ankle sprain injury risk, there have not 89 been any investigations examining their effects on the lateral ankle ligaments themselves 90 during functional sports movements commonly associated with sprain injuries. 91

The high incidence of lateral ankle ligament sprain injuries indicate that prophylactic 92 modalities have had limited success. However, accurate assessment of ankle ligament strain 93 behavior is crucial in optimizing prophylactic treatment modalities (21). Therefore, it is clear 94 95 that further investigation of these prophylactic modalities is required, which may provide important clinical information for the prevention of lateral ankle ligament sprains across 96 different athletic activities. Recent developments in musculoskeletal simulation modelling 97 techniques now allow indices of ankle ligament strain to be obtained during sports movement 98 commonly associated with ankle sprain injury (21). Therefore, the effects of different 99

prophylactic on the specific physiological parameters that cause strain parameters can now beexplored, which will be of both practical and clinical relevance.

102 There is a lack of clarity within epidemiological literature regarding the relative risk of lateral ankle sprain injuries in male and female athletes. Indeed, Waterman et al., (2010), 103 Beynnon et al., (22) and Roos et al., (23) all demonstrated that males and females had similar 104 ankle-sprain incidence ratios. However, Ristolainen et al., (24) and Hosea et al., (25) found that 105 106 ankle injuries were most common in female athletes, yet conversely Tummala et al., (26) showed that the rate of ankle injuries was greater in males. From a biomechanical perspective, 107 108 females have been shown to exhibit increased inversion-eversion laxity during a dynamic postural control task (27), reduced inversion and increased eversion during a 45° cutting 109 movement (28) and increased inversion during side-step and jump landing tasks (29). However, 110 owing to a lack of appropriate musculoskeletal modelling tools it is currently unknown whether 111 there are sex differences in lateral ligament strain characteristics (27). Thus, with the advent of 112 more advanced musculoskeletal simulation-based modeling approaches there is a clear need to 113 further investigate the mechanics of the lateral ankle ligaments in both males and females in 114 disciplines/movements commonly associated with ankle ligament strain injuries. 115

Therefore, the aims of the current investigation by using a four-experiment musculoskeletal simulation-based approach were (whilst measuring ankle kinetics, kinematics and lateral ankle ligament strain parameters to investigate): 1. sex differences during functional sports movements, 2. the effects of different court based (court, trainer and energy return) footwear during a change of direction task 3. the effects of high and low-cut court footwear during functional sports movements 4. the effects of an ankle brace and ankle sleeve during a change of direction task.

123 In relation to the aforementioned aims, the current investigation tests the following 124 hypotheses; 1. no sex differences in ankle inversion, joint loading and lateral ankle strain 125 characteristics will be evident; 2. court footwear will exhibit reduced ankle inversion, joint 126 loading and lateral ankle strain characteristics; 3. high-cut footwear will reduce ankle inversion 127 parameters, joint loading and lateral ankle strain characteristics and 4. ankle bracing will 128 attenuate ankle inversion, joint loading and lateral ankle strain characteristics.

129 Methods

For each of the four investigations, participants provided written informed consent and ethical approval was obtained from the University of Central Lancashire, in accordance with the principles documented in the Declaration of Helsinki. All participants were free from lower extremity musculoskeletal pathology at the time of data collection and had not undergone surgical intervention at the ankle joint.

135 <u>Experiment 1</u>

136 *Participants*

Fifteen male (age 30.1 ± 5.2 years, height 1.75 ± 0.07 m and body mass 77.1 ± 10.8 kg) and fifteen female (age 29.6 ± 5.6 years, height 1.66 ± 0.06 m and body mass 65.8 ± 9.9 kg) recreational athletes volunteered to take part in the current investigation.

140 *Procedure*

Participants completed five trials of three sport-specific movements, (run, one legged hop and 141 45° cut) and the order in which participants performed each movement was counterbalanced. 142 To ensure consistency, each participant wore the same footwear (Asics, Patriot 6). Kinematic 143 information was obtained using an eight-camera motion capture system (Qualisys Medical AB, 144 Goteburg, Sweden) with a capture frequency of 250 Hz. To measure ground reaction forces 145 (GRF), an embedded piezoelectric force platform (Kistler National Instruments, Model 146 9281CA) operating at 1000 Hz was adopted. The GRF and kinematic information were 147 synchronously obtained using an analogue board and interfaced using Qualisys track manager. 148

To define the anatomical frames of the thorax, pelvis, thighs, shanks and feet, passive 149 retroreflective markers of 19mm diameter were placed at the C7, T12 and xiphoid process 150 landmarks and also positioned bilaterally onto the acromion process, iliac crest, anterior 151 superior iliac spine (ASIS), posterior super iliac spine (PSIS), medial and lateral malleoli, 152 medial and lateral femoral epicondyles, greater trochanter, calcaneus, first metatarsal and fifth 153 metatarsal. The hip, knee and ankle joint centre's were delineated according to previously 154 155 established guidelines (30-32). Carbon-fibre tracking clusters comprising of four non-linear retroreflective markers were positioned onto the thigh and shank segments. The foot segments 156 157 were tracked via the calcaneus, first and fifth metatarsal, the pelvic segment using the PSIS and ASIS markers and the thorax via the T12, C7 and xiphoid markers. Static calibration trials were 158 obtained with the participant in the anatomical position in order for the positions of the 159 160 anatomical markers to be referenced in relation to the tracking clusters/markers, following which those not required for dynamic data were removed. The Z (transverse) axis was oriented 161 vertically from the distal segment end to the proximal segment end. The Y (coronal) axis was 162 oriented in the segment from posterior to anterior. Finally, the X (sagittal) axis orientation was 163 determined using the right-hand rule and was oriented from medial to lateral. 164

165

166 Data were collected during the cut and hop movements according to below procedures:

167 <u>Run</u>

Participants ran at 4.0 ± 0.2 m/s and struck the force platform with their right (dominant) limb. The average velocity of running was monitored using infra-red timing gates (SmartSpeed Ltd UK), and the stance phase of running was defined as the duration over > 20 N of vertical force was applied to the force platform. Participants completed 45° sideways cut movements using an approach velocity of 4.0 ± 0.2 m/s striking the force platform with their right (dominant) limb. Cut angles were measured from the centre of the force plate and the corresponding line of movement was delineated using masking tape so that it was clearly evident to participants. The stance phase of the cut movement was defined as the duration over > 20 N of vertical force applied to the force platform.

179 <u>Hop</u>

Participants began standing by on their dominant limb, they were then requested to hop forward maximally, landing on the force platform with same leg without losing balance. The arms were held across the chest to remove arm-swing contribution. The landing phase of the this movement was analysed which was defined as the duration from foot contact (defined as ≥ 20 N of vertical force applied to the force platform) to maximum knee flexion. The hop distance for each participant was established during practice trials, and the starting position was marked using masking tape.

187 *Processing*

Dynamic trials were digitized using Qualisys Track Manager (Qualisys Medical AB, Goteburg, 188 Sweden) in order to identify anatomical and tracking markers then exported as C3D files to 189 Visual 3D (C-Motion, Germantown, MD, USA). All data were linearly normalized to 100 % 190 of the stance/ landing phases. GRF data and marker trajectories were smoothed with cut-off 191 192 frequencies of 50 Hz at 12 Hz respectively, using a low-pass Butterworth 4th order zero lag filter. Within Visual 3D ankle were quantified using an XYZ cardan sequence (where X is 193 dorsiflexion-plantarflexion; Y is inversion-eversion and is Z is internal-external rotation). 194 Three-dimensional angular kinematic measures that were extracted in each of the 195 aforementioned planes of rotation were peak angle, peak angular velocity and minimum 196 angular velocity. Finally, within Visual 3D three dimensional joint moments were quantified 197

using Newton-Euler inverse dynamics and the peak joint moment (Nm/kg) and the joint moment impulse (Nm/kg·s) (using a trapezoidal function) were extracted for analysis. Finally, the peak translation coefficient of friction (μ) of each footwear was determined from the ratio of horizontal and vertical force components during the initial period of shoe motion (33). The peak rotational moment of the ground reaction force (Nm/kg) was used to describe the rotational friction characteristics of the footwear (34).

204 Following this, data during the stance/ landing phases were exported from Visual 3D into OpenSim 3.3 software (Simtk.org). The standard OpenSim Gait2392 musculoskeletal 205 model with 12 segments, 19 degrees of freedom and 92 musculotendon actuators was adapted 206 207 to include the three lateral ankle ligaments (ATFL, CFL and PTFL) (Figure 1). The model 208 ligament insertion points were implemented in accordance with Golano et al., (6) and the resting ligament lengths (ATFL = 22.10mm, CFL = 31.71mm and PTFL = 21.39mm) compare 209 well with the published in-vivo ligament data provided by Zhang et al., (21). The model firstly 210 was scaled to account for the anthropometrics of each participant, then as muscle forces are the 211 main determinant of joint forces (35), muscle kinetics were quantified using static optimization. 212 213 From the static optimization procedure kinetics of the muscles within the model that cross the ankle joint (extensor digitorum longus, extensor hallucis longus, flexor digitorum longus, 214 215 flexor hallucis longus, lateral gastrocnemius, medial gastrocnemius, peroneus brevis, peroneus longus, peroneus tertius, soleus, tibialis anterior, tibialis posterior) were analyzed. From these 216 muscles the peak force (BW) and the impulse (BW·ms) (using a trapezoidal function) during 217 the stance/ landing phases were obtained. Three-dimensional ankle joint forces were then 218 calculated using the joint reaction analyses function using the muscle forces generated from 219 220 the static optimization process as inputs. From the joint reaction process peak threedimensional joint forces (BW) and impulses (BW·s) (using a trapezoidal function) during the 221 stance/ landing phases were extracted. 222

@@@FIGURE 1 NEAR HERE@@@

ATFL, CFL and PTFL kinematics during each movement were calculated via the muscle analyses function within OpenSim. Peak ligament strain (%) was calculated and extracted by dividing the change in length of each ligament during movement by its resting length then multiplying by 100 to create a percentage. In addition, the peak strain velocity (%/s) was calculated and extracted as the maximum change in strain between adjacent data points using a first derivative function.

Following this, three-dimensional ankle joint kinematics, joint moments, joint forces, muscle forces, ligament strain and ligament strain velocity were extracted during the entire stance/landing phase and time normalized to 101 data points using linear interpolation for each participant (36).

234 *Statistical analyses*

Differences across the stance/ landing phase of each movement were examined using 1-235 dimensional statistical parametric mapping (SPM) (MATLAB, MathWorks, Natick, USA) 236 using the source code available at http://www.spm1d.org/. Differences between males and 237 females were examined using independent t-tests (SPM t) and the alpha level for statistical 238 significance was set at 0.05. For discrete parameters means and standard deviations were 239 calculated, and differences examined using Bayesian independent samples t-tests with default 240 prior scales using JASP software 0.10.2 (37). Bayesian factors (BF) were used to explore the 241 extent to which the data supported the alternative (H₁) hypothesis. Bayes factors were 242 interpreted in accordance with the recommendations of Jeffreys, (38), with values above 3 243 indicating sufficient evidence in support of H₁. 244

245 Experiment 2

246 *Participants*

247	Ten male recreational athletes volunteered to take part in the current investigation. The mean
248	characteristics of the participants were: age 24.6 \pm 2.8 years, height 1.77 \pm 0.05 m and body
249	$mass 73.7 \pm 7.1 kg.$
250	Footwear
251	The footwear used during this study consisted of a conventional Trainer (New Balance 1260
252	v2), Court shoes (Hi-Tec Indoor Lite), and Energy return footwear (Adidas energy boost) (shoe
253	size 8–10 in UK men's sizes) (Figure 2abc).
254	@@@FIGURE 2 NEAR HERE@@@
255	Procedure
256	Kinematic information was obtained using the procedure and biomechanical modelling
257	approach outlined in experiment 1. For this experiment participants performed maximal 180°
258	cutting maneuvers in each footwear condition (Court, Energy return and Trainer) whilst
259	striking the force platform with their dominant foot. Participants commenced their trials 6 m
260	away from the force platform, ran straight and planted their dominant foot on the force
261	platform, and then changed direction to move 180° to their initial direction of motion. The
262	order in which participants performed in each footwear condition was counterbalanced and to
263	ensure that participants utilized a similar approach velocity, their approach velocity during the
264	first trial was calculated and a maximum deviation of 5% from this was allowed (Sinclair &
265	Stainton, 2017).
266	Processing
267	The same processing techniques as experiment 1 were adopted and peak ligament strain, peak
268	ligaments strain velocities, peak angles, peak angular velocities, peak joint moments, joint
269	moment impulses, coefficient of friction, peak muscle forces, muscle force impulses, peak joint
270	forces and joint force impulses were extracted for each experimental condition.
271	Statistical analyses

272 SPM was implemented in a hierarchical manner, analogous to one-way repeated measures 273 ANOVA with post-hoc paired t-tests (SPM t) in the event of a main effect to explore differences 274 between footwear conditions. examined using (SPM t) and the alpha level for statistical 275 significance was set at 0.05. Differences in discrete parameters were examined using Bayesian 276 one-way repeated measures ANOVA, followed by Bayesian paired t-tests in the event of a 277 main effect to explore differences between footwear.

278 Experiment 3

279 Participants

Ten male recreational athletes volunteered to take part in the current investigation. The mean characteristics of the participants were: age 24.3 ± 4.1 years, height 1.77 ± 0.07 m and body mass 78.7 ± 7.4 kg.

283 *Footwear*

The footwear used during this study consisted of a conventional Trainer (New Balance 1260 v2), high-cut (Nike Lebron XII High) and low-cut (Nike Lebron XII Low) (shoe size 8–10 in UK men's sizes) (Figure 3abc).

287

@@@FIGURE 3 NEAR HERE@@@

288 Procedure

Kinematic information was obtained using the procedure and biomechanical modelling 289 approach outlined in experiment 1. For this experiment participants performed four different 290 291 movements (run, cut, change of direction and vertical jump) in each of the aforementioned footwear conditions (High, Low and Trainer). The run, cut and change of direction movements 292 were examined as described in experiments 1 and 2. For the vertical jump movement, 293 294 participants completed counter movement vertical jumps in which they were required to use full arm swing and also to commence and land the jump on the force platform. The landing 295 phase of the jump movement was quantified and was considered to have begun at foot contact 296

(defined as > 20 N of vertical force applied to the force platform) and ended at the instance of
maximum knee flexion.

299 *Processing*

The same processing techniques as experiment 1 were adopted and peak ligament strain, peak ligaments strain velocities, peak angles, peak angular velocities, peak joint moments, joint moment impulses, coefficient of friction, peak muscle forces, muscle force impulses, peak joint forces and joint force impulses were extracted for each experimental condition.

304 *Statistical analyses*

To examine differences between footwear the same statistical analyses as experiment 2 were adopted, with the same statistical principles and reporting as experiment 1 adhered to.

307 Experiment 4

308 *Participants*

Twelve male recreational athletes volunteered to take part in this study. The mean characteristics of the participants were: age 20.7 ± 1.6 years, height 1.81 ± 0.05 m and body mass 79.3 ± 8.2 kg.

312 Ankles braces

The ankle braces used during this study consisted of an ankle Sleeve (Compex, Trizone) and
also an ankle Brace (Aircast A60 DJO), in sizes small, medium and large.

315

@@@FIGURE 4 NEAR HERE@@@

316 *Procedure*

Kinematic information was obtained using the procedure and biomechanical modelling
approach outlined in experiment 1. For this experiment participants performed a 45° cutting
maneuvers as described in experiment 1 in each ankle brace condition (ankle Sleeve, ankle
Brace and no-brace).

321 Processing

The same processing techniques as experiment 1 were adopted and peak ligament strain, peak ligaments strain velocities, peak angles, peak angular velocities, peak joint moments, joint moment impulses, peak muscle forces, muscle force impulses, peak joint forces and joint force impulses were extracted for each experimental condition.

326 *Statistical analyses*

To examine differences between ankle brace conditions the same statistical analyses as experiment 2 were adopted, with the same statistical principles and reporting as experiment 1 adhered to.

330 **Results**

Tables 1-7 and supplemental figures 1-7 show comparisons between experimental conditions

in discrete parameters using Bayesian analyses and SPM. In the interests of conciseness and

clarity to the reader, only discrete values that exhibited a Bayes factor in excess of 3 and SPM

334 comparisons that demonstrated statistical significance.

335 Experiment 1

336 *Cut*

337 Statistical parametric mapping

No significant (p>0.05) differences between males and females were detected using SPM.

339 *Discrete parameters*

340 Differences between males and females in discrete parameters and the associated BF's are341 presented in table 1.

- 342 @@@TABLE 1 NEAR HERE@@@
- 343 *Run*
- 344 Statistical parametric mapping

No significant (p>0.05) differences between males and females were detected using SPM.

346 *Discrete parameters*

- None of the discrete parameters were associated with a BF greater than 3.
- 348 *Hop*

349 *Statistical parametric mapping*

Posterior force was shown to be significantly greater in males from 0-60% of the landing phase

351 **in comparison to females** (Supplemental figure 1).

352 *Discrete parameters*

Differences in discrete parameters between males and females and the associated BF's are presented in table 1.

355 <u>Experiment 2</u>

356 *Statistical parametric mapping*

Inversion was shown to be significantly greater in the trainer from 15-40% and in the court 357 footwear from 5-20% of the stance phase compared to energy return (Supplemental figure 2ab). 358 Internal rotation was shown to be significantly greater in the energy return footwear from 20-359 40% and 5-50% of the stance phase compared to the trainer and court footwear and in the 360 trainer compared to court footwear from 15-40% of the stance phase (Supplemental figure 361 2cde). Inversion velocity was greater in the court footwear from 5-10 and 90-95% but greater 362 in the energy return condition from 20-25 and 40-45% of the stance phase (Supplemental figure 363 2f). In addition, anterior force was greater in the energy return from 5-40% and compressive 364 force from 20-30% of the stance phase compared to court footwear (Supplemental figure2gh). 365 Medial forces were shown to be larger in the court footwear from 20-50 and 40-50% of the 366 stance phase compared to the energy return and trainer conditions (Supplemental figure2ij). 367 Similarly, CFL strain velocity was shown to be larger in the court footwear from 10-20 and 15-368 20% of the stance phase compared to the energy return and trainer conditions (Supplemental 369 figure2kl). Similarly, PTFL strain velocity was shown to be larger in the court footwear from 370

10-30 and 15-30% of the stance phase compared to the energy return and trainer conditions(Supplemental figure3ab).

373 *Discrete parameters*

Differences in discrete parameters between footwear and the associated BF's for the both maineffect and post-hoc analyses are presented in table 2.

376

@@@TABLE 2 NEAR HERE@@@

377 Experiment 3

378 *Change of direction*

379 Statistical parametric mapping

Inversion shown to be larger in the high footwear from 20-80 and 10-80% of the stance phase 380 compared to the low and trainer conditions (Supplemental figure 4ab). Internal rotation was 381 shown to be greater in the trainer from 40-45% of the stance phase compared to the high 382 footwear and in the low compared to the high footwear from 5-15 and 50-55% of the stance 383 phase (Supplemental figure 4cd). Inversion velocity was shown to be larger in the high 384 footwear from 5-20 and 5-10% of the stance phase compared to the low and trainer conditions 385 (Supplemental figure 4ef). In addition, the transverse plane moment was shown to be larger in 386 the high footwear from 15-20 and 15-20/25-30% of the stance phase compared to the low and 387 trainer conditions (Supplemental figure 4ef). Similarly, anterior forces were shown to be larger 388 in the high footwear from 80-85 and 70-80% of the stance phase compared to the low and 389 390 trainer conditions (Supplemental figure 4ij).

391 *Discrete parameters*

392 Differences in discrete parameters between footwear and the associated BF's for the both main393 effect and post-hoc analyses are presented in table 3.

394

@@@TABLE 3 NEAR HERE@@@

395 *Cut*

396 *Statistical parametric mapping*

Inversion velocity shown to be larger in the high footwear from 10-20% of the stance phase 397 compared to the low conditions (Supplemental figure 5a). External rotation velocity was also 398 shown to be greater in the high footwear compared to low from 10-15% of the stance phase 399 (Supplemental figure 5b). In addition, the transverse plane moment was shown to be larger in 400 the high footwear from 5-10 of the stance phase compared to the low condition (Supplemental 401 402 figure 5c). Similarly, the lateral gastrocnemius force was shown to be larger in the high footwear from 50-65 of the stance phase compared to the low condition (Supplemental figure 403 404 5d). Finally, ATFL strain was shown to be larger in the trainer compared to the low condition from footwear from 80-100% of the stance phase (Supplemental figure5e). 405

406 *Discrete parameters*

407 Differences in discrete parameters between footwear and the associated BF's for the both main408 effect and post-hoc analyses are presented in table 4.

409

@@@TABLE 4 NEAR HERE@@@

410 *Run*

411 Statistical parametric mapping

Plantarflexion velocity was shown to be larger in the trainer from 70-100 and 70-95% of the 412 stance phase compared to the high and low footwear conditions (Supplemental figure 6ab). 413 Eversion velocity was also shown to be greater in the high footwear compared to the trainer 414 415 from 0-10% of the stance phase (Supplemental figure 6c). In addition, compressive forces were larger in the high footwear from 30-35 and 5-10/20-25/60-65% of the stance phase compared 416 to the trainer and low footwear conditions (Supplemental figure 6de). ATFL strain was shown 417 to be larger in the trainer from 95-100 and 95-100% of the stance phase compared to the high 418 and low footwear conditions (Supplemental figure 6fg). Similarly, ATFL strain velocity was 419 larger in the trainer from 75-100 and 75-100% of the stance phase compared to the high and 420

421	low footwear conditions (Supplemental figure 6hi). Finally, PTFL strain velocity was shown
422	to be greater in the high compared to the low footwear from 10-30/ 85-100% of the stance
423	phase (Supplemental figure 6j).
424	Discrete parameters
425	Differences in discrete parameters between footwear and the associated BF's for the both main
426	effect and post-hoc analyses are presented in table 5.
427	@@@TABLE 5 NEAR HERE@@@
428	Vertical jump
429	Statistical parametric mapping
430	Flexor digitorum longus force was shown to be larger in the high footwear from 30-40% of the
431	stance phase compared to the trainer (Supplemental figure 7a). Similarly, flexor hallucis longus
432	force was greater in the high footwear from 35-40% of the stance phase compared to the trainer
433	(Supplemental figure 7b).
434	Discrete parameters
435	Differences in discrete parameters between footwear and the associated BF's for the both main
436	effect and post-hoc analyses are presented in table 6.
437	@@@TABLE 6 NEAR HERE@@@
438	Experiment 4
439	Statistical parametric mapping
440	Inversion was shown to be larger in the sleeve compared to the brace from 35-85% of the stance
441	phase and in the no-brace condition compared to the sleeve from 15-15% of the stance phase
442	(Supplemental figure 8ab). Medial forces were also larger in the no-brace condition compared
443	to brace from 15-20% of the stance phase (Supplemental figure 8c).

Discrete parameters

- 445 Differences in discrete parameters between footwear and the associated BF's for the both main446 effect and post-hoc analyses are presented in table 7.
- 447

@@@TABLE 7 NEAR HERE@@@

448 **Discussion**

The current investigation using a four-experiment approach represents the first study to explore differences in ankle kinetics, kinematics and lateral ankle ligament strain parameters between males and females in addition to examining the influence of different footwear and ankle brace conditions. A study of this nature provides further insight into potentially distinct incidence rates of lateral ankle ligament injures in female/males athletes, in addition to the potential efficacy of different prophylactic modalities for the prevention of ankle ligament pathologies in different sports movements.

The findings from experiment 1 do not support hypothesis 1, as differences in ankle 456 inversion, joint loading and lateral ankle strain characteristics were evident during both the cut 457 and hop movements. Specifically, both discrete parameters and SPM showed that males were 458 associated with enhanced inversion velocity, peak posterior force and ATFL strain rate 459 compared to females. Increased ligament strain magnitudes are linked to the aetiology of lateral 460 ankle ligament pathology, either as an acute occurrence or through repeated manifestations/ 461 exposures (12). Similarly, enhanced ankle joint loading is associated, through repeated 462 exposure with the initiation and progression joint osteoarthritic degeneration (40). Therefore, 463 experiment 1 collectively indicates that males are most susceptible to the mechanisms linked 464 to the aetiology of lateral ankle ligament and joint pathologies compared to females. 465

Importantly, in partial support of hypothesis 2 the findings from experiment 2 showed via both discrete parameters and SPM that the energy return footwear were associated with enhanced ankle joint loading in all three planes in comparison primarily to the court footwear, although medially directed forces were also greater compared to the trainer during early and 470 midstance. Because of the proposed association between contact loading and the initiation/ 471 progression of joint degeneration (40), this observation may be clinically meaningful. It can be 472 conjectured based on the findings from this investigation that the specific energy return 473 footwear examined in this investigation may increase the risk from degenerative ankle joint 474 injury during sport specific change of direction movements.

Further to this however, in contradiction of hypothesis 2, both discrete parameters and 475 476 SPM showed that the court footwear were found to be enhance both CFL and PTFL velocity compared to both the energy return and trainer conditions. Taking into account the concurrent 477 478 increases in inversion and inversion velocity in the court footwear this observation was to be expected as excessive inversion itself is recognized as a primary kinematic mechanism 479 associated with ankle sprain injuries (12). One of the main functions of the lateral ligaments is 480 to resist inversion (9) and importantly the in-vivo data of Zhang et al., (21) showed that both 481 the CFL and PTFL are lengthened by inversion. In addition, it has been ventured that friction 482 at the shoe surface interface influences the risk for lateral ankle sprain injuries (41). However, 483 the findings from experiment 2 indicate that whilst the coefficient of friction was reduced in 484 the court footwear, the rotational moment was enhanced. This observation concurs with those 485 of Sinclair & Stainton, (36) in that the rotational moment rather than the coefficient of friction 486 were enhanced in court footwear and that it is this parameter that most strongly influences soft 487 tissue injury risk during change of direction tasks. Regardless, the enhanced ligament strain 488 489 observation in the court footwear may be clinically meaningful, as the aetiology of lateral ankle ligament injury is considered to be mediated through enhanced ligamentous strain 490 characteristics (12). Experiment 2 therefore indicates that the biomechanical mechanisms 491 responsible for lateral ankle ligament strain injuries were enhanced in the court specific 492 footwear; a concerning observation taking into account that change of direction movements are 493 fundamental to court-based activities (36). 494

In contradiction to hypothesis 3, collective consideration of the observations from 495 experiment 3 in relation to joint loading showed using both SPM and discrete parameters that 496 the high cut footwear enhanced joint loading in all three planes during the change of direction, 497 cut and run movements in comparison primarily to both the low and trainer conditions. As 498 such, taking into account the aforementioned association between joint loading and the 499 aetiology of joint degeneration (40), the findings from experiment 3 indicate that high cut 500 501 footwear may enhance the risk from degenerative ankle joint injury during sport specific movements. Furthermore, in partial support of hypothesis 3 ATFL strain parameters were 502 503 shown to be enhanced in the trainer compared to the high and low conditions in the run movement and the high footwear for the cut movement. However, conversely PTFL strain 504 characteristics were greater in the high-cut footwear for the run and vertical jumps movement 505 506 and both high and low-cut conditions during the cut. The aforementioned results can also be contextualized taking into account the in-vivo observations of Zhang et al., (21) as both the 507 discrete and SPM based findings from experiment 3 showed that inversion/ eversion 508 parameters were enhanced in the high-cut footwear and plantarflexion variables larger in the 509 trainer condition. Zhang et al., (21) showed that the ATFL is lengthened during plantarflexion 510 and eversion and that the PTFL exhibits lengthening during dorsiflexion and inversion. As 511 lateral ankle ligament sprain injuries are linked to the magnitude of the strain experienced by 512 the ligaments themselves (12), experiment 3 provides interesting observations in that the 513 514 experimental footwear affect ligament strain characteristics differently. This indicates that the trainer may enhance the risk for ATFL pathologies and the high-cut footwear condition appears 515 to increase the risk from PTFL sprain injuries. 516

517 In support of hypothesis 4, the observations from experiment 4 showed using both SPM 518 and discrete parameters that the no-brace condition was associated with enhanced medially 519 directed ankle joint loading compared to both the sleeve and brace. Importantly, excessive joint

loading is linked to the aetiology of joint degeneration, and thus the findings from experiment 520 4 indicate that the ankle sleeve and brace conditions are able to attenuate the biomechanical 521 mechanisms associated with joint pathology (40). In addition, further supporting hypothesis 4 522 it was also shown that PTFL strain was shown to be larger in the sleeve in comparison to the 523 brace condition. As the PTFL exhibits lengthening during and inversion, which was shown to 524 be concurrently enhanced in the sleeve condition this observation was to be expected (21). 525 526 Therefore, as lateral ankle ligament pathologies are associated with excessive ligamentous strain magnitudes (12), experiment 4 indicates that the brace may attenuate the biomechanical 527 528 risk factors associated with PTFL sprain injuries.

529 Limitations

A potential limitation is that musculoskeletal simulation modelling approach adopted in order 530 to quantify ligament strain mechanics was not able to account for the inter-variability in the 531 ligamentous construction and insertion points (42). Whilst should be noted that direct measures 532 are not possible in human participants and that the resting lengths of the modelled ligaments as 533 well as the strain magnitudes are consistent with those presented in the scientific literature and 534 within the physiological range (21). There is nonetheless, considerable scope for future 535 development of simulation-based models to address and improve upon these limitations; to 536 provide more accurate and individually adapted musculoskeletal simulations of lateral ankle 537 ligament mechanics linked to the aetiology of sprain injuries. 538

539 Conclusion

The findings from the current four-experiment investigation provide further insight into differences in lateral ankle ligament parameters between male and female athletes the mechanisms responsible for the potentially increased incidence of lateral ankle ligament sprain injuries in males, whilst also highlighting the prophylactic efficacy of ankle braces in attenuating the ankle strain mechanisms linked to the aetiology of lateral ankle ligamentinjuries.

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672 **Figure labels**



674 Figure 1: Lateral ankle ligaments (ATFL, CFL and PTFL) in the OpenSim based model.





Figure 2: Footwear from experiment 2 (a. = court, b. = energy return & c. = trainer).









Table 1: Mean, standard deviation and Bayes factors (BF) for experiment 1.

683

	Ma	ale	Fen	nale	<u>68</u> 4
	Mean	SD	Mean	SD	
			Cut		085
Peak transverse plane angle (°)	8.80	5.98	3.84	4.24	36835
Peak inversion velocity (°/s)	260.39	133.18	219.18	105.32	6.33
Extensor digitorum longus impulse (BW·s)	0.06	0.02	0.03	0.02	5.74
Peak peroneus longus force (BW)	1.23	0.17	1.48	0.23	1 2589
			Нор		600
Peak posterior force (BW)	2.24	0.48	1.35	0.63	166.40
Peak ATFL strain rate (%/s)	266.77	124.08	133.16	109.39	4(490)

691 Notes: Bold Bayes factors indicate that they exceed 3.

Table 2: Mean, standard deviation and Bayes factors (BF) for experiment 2.

	Trai	ner	Energy	return	Cou	urt			BF post-hoc	
	Mean	SD	Mean	SD	Mean	SD	BF Main effect	Trainer vs Energy return	Trainer vs Court	Energy return vs Court
Compressive force impulse (BW·s)	2.63	1.04	2.91	1.16	2.71	1.09	11.18	2.33	0.32	47.17
Peak medial force (BW)	0.97	0.56	1.05	0.70	0.88	0.58	23.03	0.67	1.12	13.55
Medial/lateral force impulse (BW·s)	0.18	0.10	0.21	0.13	0.15	0.12	49.92	0.69	1.04	128.10
Peak coronal plane moment (Nm/kg·s)	0.68	0.19	0.63	0.23	0.61	0.22	7.81	1.40	3.13	0.47
Peak transverse plane moment (Nm/kg·s)	0.28	0.07	0.23	0.09	0.25	0.09	27.92	31.56	0.57	1.63
Peak inversion (°)	20.93	4.92	18.01	3.83	20.52	4.23	43.60	2.64	0.32	8.98
Peak internal rotation (°)	-6.04	3.93	-5.87	3.46	-8.35	2.98	209.01	0.22	5.30	10157.19
Peak inversion velocity (°/s)	410.07	90.83	338.49	93.50	421.06	66.23	4.55	0.62	0.23	34.82
Peak internal rotation velocity (°/s)	256.81	82.32	219.11	87.98	299.27	85.55	28.13	0.49	1.46	99.93
Peak extensor digitorum longus force (BW)	0.44	0.32	0.50	0.32	0.61	0.22	108.95	0.81	8.91	4.90
Extensor digitorum longus impulse (BW·s)	67.55	69.24	83.39	81.64	86.02	72.40	573.57	4.90	235.80	0.28
Peak extensor hallucis longus force (BW)	0.13	0.10	0.17	0.12	0.19	0.10	191.84	1.53	781.61	0.65
Extensor hallucis longus impulse (BW·s)	18.61	20.21	24.67	25.26	25.18	24.62	96.84	2.87	67.01	0.23
Peak CFL strain rate (%/s)	69.07	42.26	78.81	45.45	90.86	36.19	5.34	204.79	9.41	0.49
Peak PTFL strain rate (%/s)	119.57	38.62	134.47	48.76	151.45	40.67	7.68	0.65	15.67	0.53
Coefficient of friction (µ)	0.64	0.08	0.60	0.07	0.57	0.08	665.37	3.85	15.63	5.18
Peak rotational moment (Nm/kg)	0.27	0.09	0.25	0.07	0.36	0.07	6062.27	0.42	16.20	70.53

	Hig	High Low Trainer		BF post-hoc						
	Mean	SD	Mean	SD	Mean	SD	effect	High vs Low	High vs Trainer	Low vs Trainer
Peak anterior force (BW)	-1.56	1.09	-1.68	0.84	-1.05	0.96	5.64	0.27	1.74	3.02
Peak medial force (BW)	0.99	0.63	0.71	0.35	0.88	0.39	5.61	3.92	0.36	1.76
Medial/lateral force impulse (BW·s)	0.16	0.08	0.11	0.07	0.16	0.08	5.23	11.11	0.24	1.30
Peak dorsiflexion moment (Nm/kg)	2.16	0.28	2.09	0.26	1.91	0.23	608.38	0.68	10.01	62.71
Peak internal rotation moment (Nm/kg)	0.36	0.11	0.30	0.08	0.28	0.11	2422.01	19.48	23.57	0.79
Transverse plane moment impulse (Nm/kg·s)	0.08	0.02	0.06	0.01	0.06	0.03	14.82	2.84	10.93	0.23
Peak inversion (°/s)	25.25	1.86	22.54	1.96	22.30	2.77	31.08	7485.33	5.13	0.24
Peak inversion velocity (°/s)	351.79	80.72	311.14	61.56	325.95	94.50	3.96	90.91	0.76	0.31
Peak internal rotation velocity (°/s)	-205.32	33.82	-187.38	34.61	-160.77	51.10	28.12	1.51	19.23	0.73
Peak rotational moment (Nm/kg)	0.36	0.07	0.33	0.09	0.32	0.07	3.50	3.40	1.93	0.26

Table 3: Mean, standard deviation and Bayes factors (BF) for the *change of direction* movement from experiment 3.

	High		Lov	w	Trainer			BF post-hoc		
	Mean	SD	Mean	SD	Mean	SD	effect	High vs Low	High vs Trainer	Low vs Trainer
Compressive force impulse (BW·s)	1.56	0.17	1.52	0.16	1.43	0.20	140.30	0.65	11.36	4.41
Peak internal rotation moment (Nm/kg)	0.33	0.05	0.27	0.07	0.32	0.06	9.49	4.95	0.27	3.70
Sagittal plane moment impulse (Nm/kg·s)	0.40	0.04	0.36	0.07	0.33	0.06	211.74	2.06	37.04	0.96
Peak inversion (°)	15.11	2.16	12.50	2.65	11.90	2.35	115.27	13.51	333.33	0.27
Peak dorsiflexion velocity (°/s)	396.85	105.55	409.55	121.62	358.22	94.37	229.57	0.56	18.18	6.71
Peak inversion velocity (°/s)	189.72	109.82	146.82	76.76	171.35	100.24	31.64	4.63	1.58	1.32
Peak plantarflexion velocity (°/s)	-553.44	80.56	-580.91	66.22	-600.79	78.28	9.95	2.40	14.49	0.37
Peak flexor digitorum longus force (BW)	0.19	0.06	0.18	0.10	0.14	0.06	5.45	0.26	9.01	1.64
Flexor digitorum longus impulse (BW·ms)	7.49	3.36	6.42	3.15	5.88	2.38	18.17	3.92	3.28	0.46
Peak flexor hallucis longus force (BW)	0.19	0.06	0.17	0.09	0.13	0.06	41.47	0.39	45.45	2.09
Soleus impulse (BW·ms)	588.54	114.66	561.75	121.01	480.03	153.49	3.14	0.29	1.39	3.06
Peak tibialis posterior force (BW)	0.61	0.25	0.51	0.14	0.35	0.10	1047.63	0.67	32.26	250.00
Tibialis posterior impulse (BW·ms)	41.94	30.74	27.95	15.51	14.21	4.47	42.50	1.06	4.42	8.62
ATFL peak strain (%)	6.67	3.39	5.39	4.44	8.14	3.79	16.03	0.58	1.32	7.46
Peak PTFL strain velocity (%/s)	221.55	71.61	220.29	71.42	202.05	60.73	874.96	0.24	43.48	23.26

Table 4: Mean, standard deviation and Bayes factors (BF) for the *cut* movement from experiment 3.

	Hig	gh Low		Train	er		BF post-hoc			
	Mean	SD	Mean	SD	Mean	SD	BF Main effect	High vs Low	High vs Trainer	Low vs Trainer
Peak anterior force (BW)	-2.49	0.51	-1.96	0.62	-1.95	0.32	187.85	11.49	50.00	0.23
Anterior/posterior force impulse (BW·s)	-0.12	0.10	-0.07	0.09	-0.07	0.06	13.39	4.18	6.45	0.23
Peak compressive force (BW)	9.40	1.48	8.48	1.00	8.28	1.30	28.94	4.13	4.39	0.30
Compressive force impulse (BW·s)	1.32	0.14	1.19	0.12	1.12	0.14	521.13	33.33	23.81	0.56
Sagittal plane moment impulse (Nm/kg·s)	0.36	0.07	0.32	0.06	0.29	0.07	442.99	18.87	9.62	1.05
Peak external rotation velocity (°/s)	154.11	20.81	141.41	18.13	164.13	30.27	3.40	0.95	0.33	23.26
Peak plantarflexion velocity (°/s)	-497.12	33.09	-530.79	16.75	-607.92	25.15	7928259	5.03	250000	2040.82
Peak eversion velocity (°/s)	-217.36	50.85	-208.96	62.79	-184.20	50.44	11.88	0.36	3.83	1.56
Peak lateral gastrocnemius force (BW)	0.43	0.16	0.31	0.07	0.30	0.05	49.27	2.67	5.88	0.24
Lateral gastrocnemius impulse (BW·ms)	37.20	10.90	26.30	8.60	27.30	6.74	624.50	6.80	125.00	0.26
Medial gastrocnemius impulse (BW·ms)	159.70	66.67	132.50	49.53	129.50	41.68	5.23	6.49	1.20	0.24
Peak soleus force (BW)	4.70	0.51	4.38	0.33	4.36	0.34	11.79	3.53	6.54	0.24
Soleus impulse (BW·ms)	569.40	71.12	504.10	81.00	475.70	81.89	44.60	8.77	12.82	0.36
ATFL peak strain (%)	3.61	4.02	5.87	1.99	7.86	2.89	149.87	1.31	9.52	12.50
Peak ATFL strain velocity (%/s)	345.61	25.29	362.75	16.19	392.86	11.39	4318067.79	2.04	2331.00	6622.52
Peak PTFL strain velocity (%/s)	188.01	41.03	182.46	35.72	175.60	37.13	4.99	0.39	3.00	0.63

Table 5: Mean, standard deviation and Bayes factors (BF) for the *run* movement from experiment 3.

Table 6: Mean, standard deviation and Bayes factors (BF) for the *vertical jump* movement from experiment 3.

	High		Low		Trainer			BF post-hoc		
	Mean	SD	Mean	SD	Mean	SD	effect	High vs Low	High vs Trainer	Low vs Trainer
Peak compressive force (BW)	5.00	1.08	5.59	0.95	5.25	1.27	6.37	4.72	0.63	0.63
Peak dorsiflexion (°)	22.96	7.17	24.62	7.11	25.72	8.29	3.56	1.07	16.95	0.32
Extensor digitorum longus impulse (BW·ms)	0.04	0.03	0.02	0.02	0.02	0.02	14.94	1.59	9.52	0.24
Extensor hallucis longus impulse (BW·ms)	0.01	0.01	0.01	0.00	0.01	0.01	7.24	1.37	6.76	0.25
Flexor digitorum longus impulse (BW·ms)	0.01	0.00	0.01	0.00	0.01	0.00	151.30	1.46	250.00	0.75
Peak flexor hallucis longus force (BW)	0.11	0.02	0.11	0.01	0.09	0.01	10.50	0.26	2.21	250.00
Flexor hallucis longus impulse (BW·ms)	0.01	0.00	0.01	0.00	0.01	0.01	115.76	1.07	249.00	0.90
Peroneus brevis impulse (BW·ms)	0.03	0.01	0.02	0.01	0.02	0.02	7.49	3.88	0.97	0.69
Peak tibialis posterior force (BW)	0.48	0.10	0.69	0.24	0.43	0.19	5.09	1.46	0.25	6.10
Peroneus tertius impulse (BW·ms)	0.01	0.00	0.01	0.00	0.01	0.00	81.36	3.66	18.52	0.26

Table 7: Mean, standard deviation and Bayes factors (BF) from experiment 4.

	No-brace		Sleeve		Brace			BF post-hoc		
	Mean	SD	Mean	SD	Mean	SD	BF Main effect	No-brace vs Sleeve	No- brace vs Brace	Sleeve vs Brace
Medial/lateral force impulse (BW·s)	0.16	0.06	0.14	0.06	0.12	0.09	10.20	10.55	3.08	0.55
Peak coronal plane moment (Nm/kg)	1.48	0.28	1.55	0.48	1.15	0.45	3.44	0.23	1.07	28.47
Coronal plane moment impulse (Nm/kg·s)	0.19	0.04	0.20	0.07	0.15	0.06	3.38	0.23	0.96	34.86
Peak inversion (°)	13.28	4.44	14.64	4.17	10.83	5.53	3.29	0.30	0.55	5.83
Extensor hallucis longus (BW·s)	2.98	1.74	2.79	1.45	6.59	4.65	44.09	0.24	3.16	5.08
Flexor hallucis longus impulse (BW·s)	5.31	2.27	4.83	1.64	10.46	7.14	9.82	0.35	1.86	3.06
Peroneus longus impulse (BW·s)	252.96	40.60	241.98	43.89	213.12	32.75	28.90	0.56	5.18	2.21
PTFL peak strain (%)	16.27	5.08	17.05	4.25	15.42	4.72	3.35	1.10	0.44	3.53